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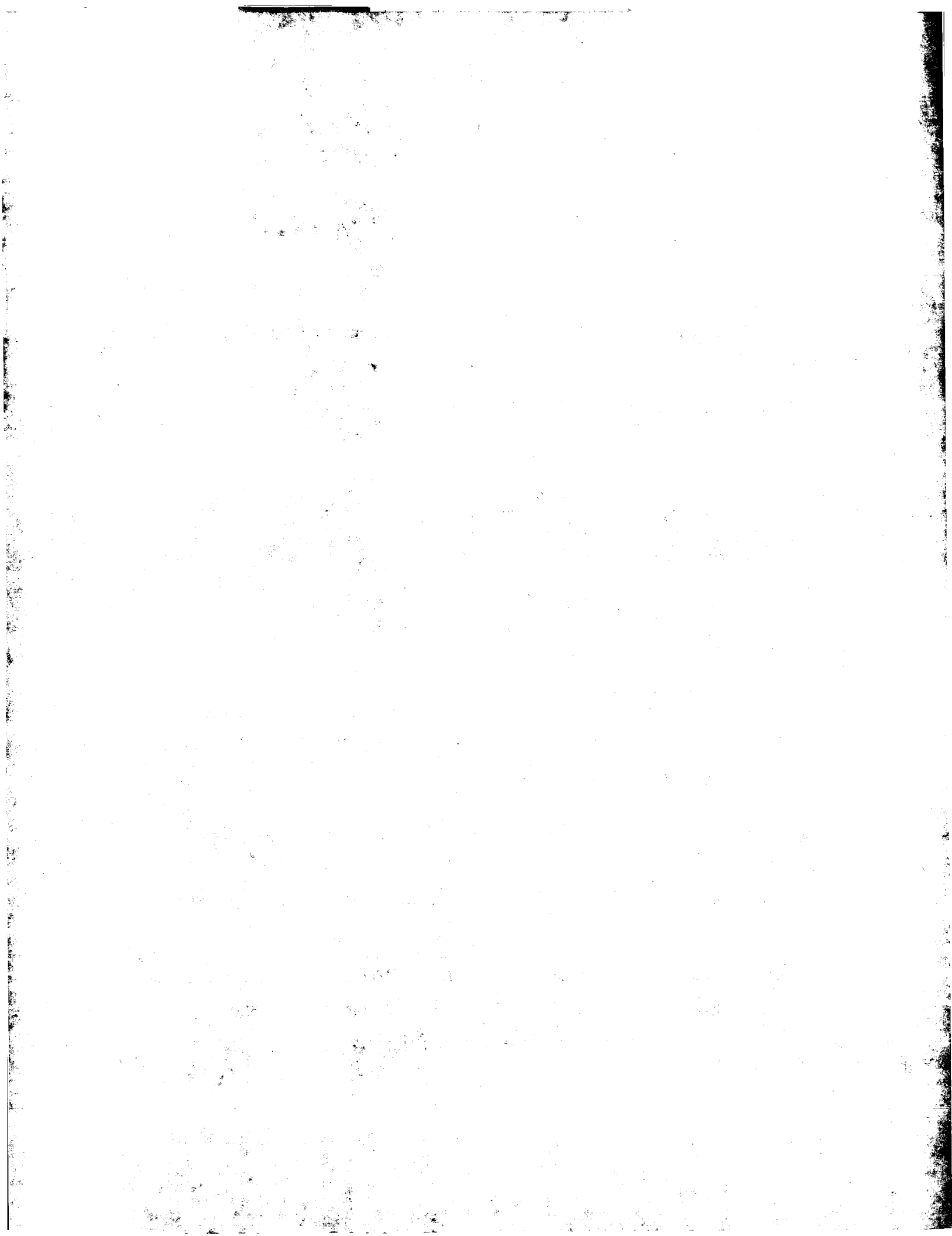
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Bistable magnetic actuator

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(72) Inventor(s)
Brian McKean
Derek Kenworthy

(73) Proprietor(s)
Brian McKean Associates Ltd

(Incorporated in the
United Kingdom)

Woodley House
Woodley Street
Ruddington
Nottingham
NG11 6EP
United Kingdom

(74) Agent and/or
Address for Service
Eric Potter Clarkson
St Mary's Court
St Mary's Gate
Nottingham
NG1 1LE
United Kingdom

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(55) Documents cited
EP0460666 A
EP0354803 A
EP0225388 A
DE003520879 C
DE003338551 A
FR002532107 A
FR001363793 A
IIS4522890 A
US3377519 A
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1989 IEEE Industry
Applications Society
Annual Meeting, 1989,
XP91581
Part 1, pages 195-202

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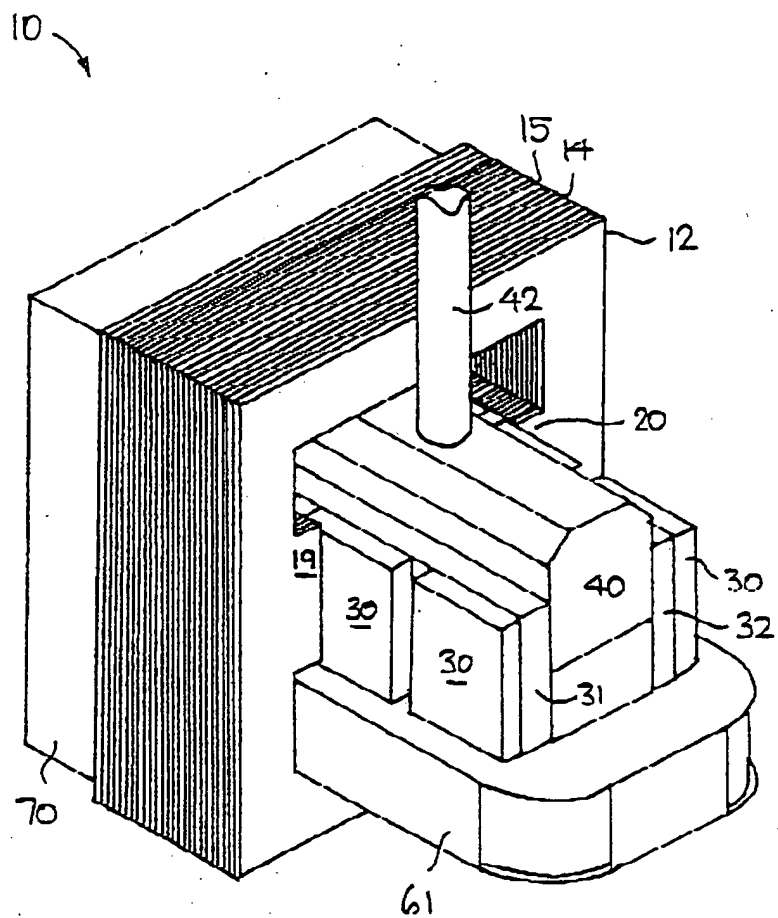


FIGURE 1

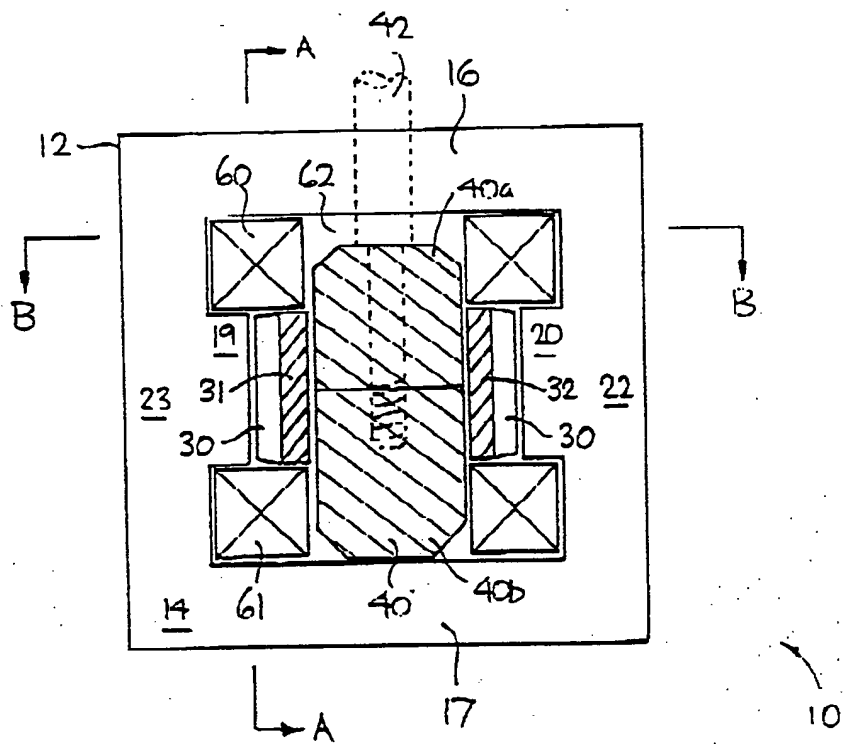


FIGURE 2

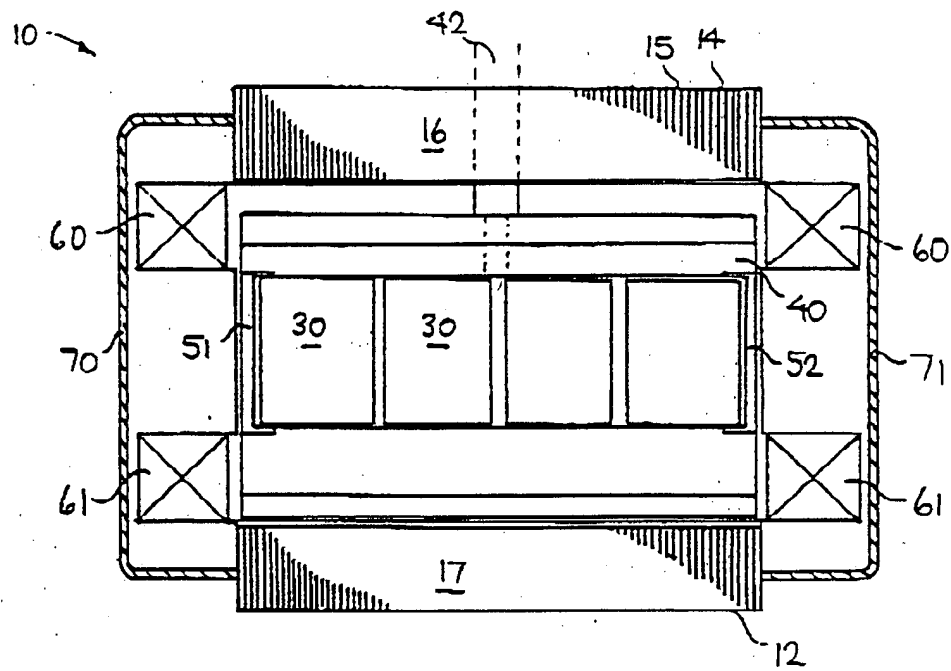


FIGURE 3

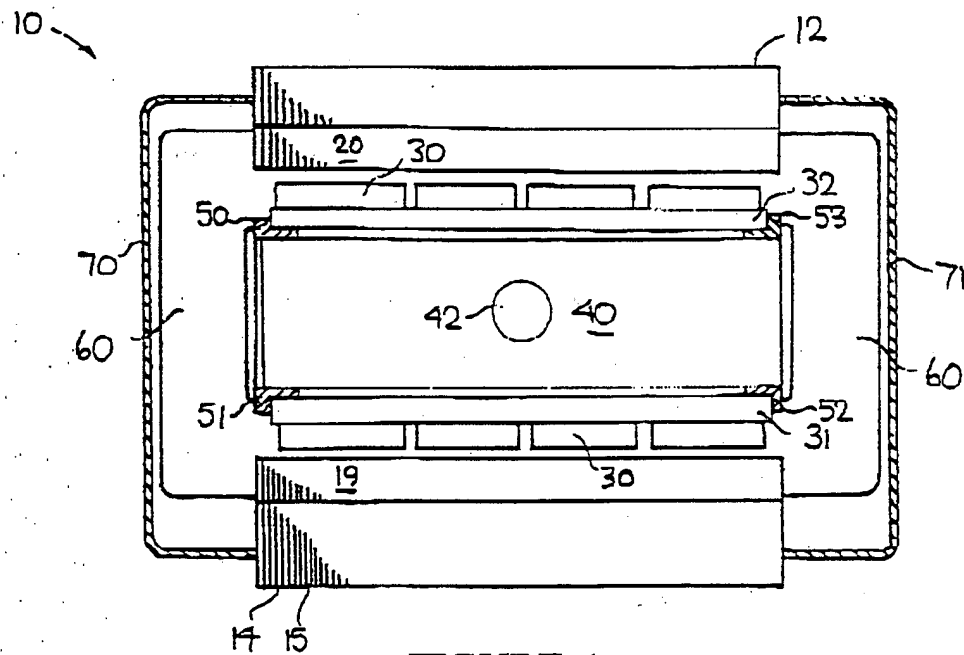


FIGURE 4

BISTABLE MAGNETIC ACTUATOR

5 The present invention relates to magnetic actuators, and in particular to actuators suitable for the operation of electric circuit breakers.

10 In all electric circuit breakers it is necessary to have a mechanism that will open and close contacts in order to interrupt or close an electric circuit.

15 Conventional high-voltage circuit breakers include mechanical systems for opening and closing the circuit breaker contacts that are very complex to build and require periodic and expensive overhaul and maintenance. The advent of modern vacuum interrupters for use in high voltage circuit breakers, requiring no maintenance or overhaul, has led to the desire to make available actuator mechanisms requiring little or no maintenance and ideally matched to the characteristics of the vacuum interrupter.

20 These characteristics typically include: short stroke of the moving contact between open and closed positions, usually of the order of 8 to 12 mm; low operating times, typically 10 milliseconds between open and closed positions during operation; high pressure force between contacts when closed to withstand electromagnetic forces during short circuits; and
25 low operating energy.

Prior art bistable permanent magnet actuators meet some of the above characteristics but typically have a number of disadvantageous features.

30

For example, in UK Patent Application No. 2112212 there is described a relay which has a bistable permanent magnet actuator. This relay includes an electromagnetic coil wound around the armature to provide the necessary electromagnetic driving force to move the actuator
5 between the two bistable positions. This design has a number of disadvantages, not least that the flux generated by the coil works in opposition to the permanent magnet flux, thus having a tendency to destroy the permanent magnets in time. Additionally, considerable flux must be generated to oppose and overcome the permanent magnet flux,
10 and the movement of the actuator is thus rapid and substantially uncontrolled. These types of device are inherently unsuitable for actuators requiring large holding forces, as they will suffer considerable damage when electromagnetic fluxes large enough to overcome the permanent magnet flux are generated. They thus have application only in lower
15 power rôles. In addition, the coil is mounted on the moving part (the actuator) thereby requiring a more complex and less reliable configuration.

In a further example, UK Patent Application No. 2223357 there is described a bistable, magnetically actuated circuit breaker. This device
20 includes a dual yoke construction, each yoke providing either the low reluctance permanent magnet flux path or the high reluctance path of the bistable configuration. The permanent magnet is housed between two halves of the actuator. Actuation is provided by one of two electromagnetic coils which operate to destabilise the armature without
25 substantially reducing the flux in the permanent magnet. A substantial disadvantage of this device is that the magnet is located in the armature, and thus for actuators requiring large holding forces, is prone to physical damage under the impact of switching the armature position. A further substantial disadvantage of this device is that the conduction of permanent
30 magnet flux around the device is inefficient and large magnets are required

to achieve reasonable holding force. Similarly, generation of electromagnetic flux is inefficient and large switching currents are required.

5 Where prior art designs of actuator have been made to accommodate high power circuit breakers requiring large holding forces, it has always been necessary to provide electromagnetic coils capable of generating very large opposing fluxes in order to switch the actuator from one bistable position to the other. While this is not always a problem, it
10 is particularly difficult where the breakers must have an independent source of power in order to switch, such as those which must be powered by integral batteries which are required to have a long, maintenance-free life. In addition, the use of high power coils necessarily increases the size of the actuators, and may necessitate expensive cooling mechanisms where
15 frequent switching occurs.

There is therefore a need to provide a permanent magnet actuator which is simple and cheap to manufacture, suitable for use with high power applications generating large holding forces, with substantially
20 lower power consumption than known systems, and easily configurable to a variety of specifications.

In accordance with one aspect of the present invention, there is provided a bistable permanent magnet actuator comprising:

- 25 a magnetic yoke having a laminated structure;
 at least one permanent magnet; and
 an armature axially reciprocable in a first direction within the yoke;
the actuator configured to provide:
 a first low reluctance flux path and a first high reluctance flux path
30 when the armature is in a first position;
 a second low reluctance flux path and a second high reluctance flux path when the armature is in a second position;

means to drive the armature between the first and second positions;
characterized in that:

each laminate of the yoke defines a plane in which a portion of the permanent magnet and armature reside, and wherein the configuration of the actuator thereby enables an increase in the permanent magnet flux flowing through the actuator by the addition of further yoke laminations and a corresponding increase in the linear dimension of the magnet and armature in a second direction perpendicular to the plane of the laminations.

10

In accordance with a further aspect of the present invention, there is provided a method of manufacturing a bistable permanent magnet actuator comprising the steps of:

constructing a magnetic yoke from a plurality of laminations each configured to form a part of a magnetic circuit with at least one permanent magnet and an armature axially reciprocable in a first direction within the yoke;

configuring the actuator to provide a first low reluctance flux path and a first high reluctance flux path when the armature is in a first position and a second low reluctance flux path and a second high reluctance flux path when the armature is in a second position;

providing means to drive the armature between the first and second positions; and

using a predetermined number of laminations to expand the device in a linear direction orthogonal to the plane of the yoke laminations, and increasing the corresponding linear dimension of the magnet(s) and armature in order to increase in the permanent magnet flux flowing through the actuator to achieve the desired specification of actuator.

30

Embodiments of the present invention will now be described by way of example, and with reference to the accompanying drawings in which:

Figure 1 shows a perspective view of part of a magnetic actuator in accordance with one embodiment of present invention, with one coil and yoke laminations removed to reveal internal components;

5 Figure 2 shows an end view of a centre cross-section of the complete actuator of figure 1;

Figure 3 shows a side view on cross-section A—A of the actuator of figure 2, but with the leading part of both coils removed for clarity;

10

Figure 4 shows a top view on cross-section B—B of the actuator of figure 2, but with the upper coil removed for clarity.

With reference to the figures, a bistable, permanent magnet actuator
15 is shown generally as 10. The actuator comprises an outer yoke 12, which is composed of a number of laminations 14,15 formed of a suitably high magnetic permeability material, for example steel sheets. Each lamination has an upper and a lower pole portion 16,17 and preferably includes a pair of centre arms 19,20 projecting inwards from side portions
20 22,23. Although the preferred embodiment has been shown as symmetrical about a vertical centre line on figure 2, it will be understood that one of the side portions 22,23 could be omitted.

Within the laminations 14,15 of yoke 12, and preferably lying
25 between and adjacent to centre arms 19,20 are a number of permanent magnets 30. Magnets 30 are attached to a pair of inner yokes 31,32 which are spaced from an armature 40 which is reciprocally mounted within the assembly in order that it may slide between a first, lower position in which the lower face of the armature 30 is in contact with the
30 lower pole portion 17 of yoke 12 as shown in figure 2, and a second

upper position in which the armature is in contact with the upper pole portion 16 of yoke 12. Coaxial with the armature 40 is an actuator rod 42 shown in dotted outline on the figures. Four bearing plates 50...53 (see figures 3 and 4) are positioned between the ends of inner yokes 31,32 and the armature 40 to facilitate smooth linear movement of the armature within the yokes.

A pair of coils 60,61 circumscribe the upper and lower portions of armature 40 respectively. The coils are preferably mounted within the recesses formed between the poles 16,17 of the yoke 12 and the centre arms 19,20. The whole assembly may then be bolted together and provided with end caps 70,71.

With the armature 40 in the position as shown in the figures, a low reluctance magnetic circuit is formed by the magnet 30, the lower half of side portion 22 of yoke 12, the lower pole 17 of yoke 12, the lower half of armature 40 and the inner yoke 32. A high reluctance magnetic circuit is formed by magnet 30, the upper half of side portion 22 of yoke 12, the upper pole 16 of yoke 12, the upper half of armature 40 and the inner yoke 32. Corresponding circuits are replicated on the left half of the actuator as viewed in figure 2.

In this position, a strong permanent magnet flux is present in the low reluctance circuit which holds the armature in the lower position. Little flux is present in the high reluctance circuit due to the air gap 62 present between the upper part of the armature 40 and the upper pole 16 of the yoke 12. However, it will be recognized that the temporary application of a current of appropriate polarity in upper coil 60 will cause a high flux to be forced across the air gap 62, providing an upward motive force on armature 40 in order to close the air gap. Providing the flux

induced by coil 60 is greater than the flux present in the low reluctance circuit, the armature will be "flipped" to an upper position; thus swapping over the high and low reluctance circuits described *supra*.

5 The armature may be returned to its first bistable position by analogous use of the lower coil 61.

10 This action offers considerable improvement over some types of actuator in that the coils never serve to oppose the permanent magnet flux, and thus do not tend to destroy the permanent magnets over time.

15 The use of an outer yoke 12 comprised of a number of laminations has several important advantages. Firstly, the permanent magnet flux flowing through the low reluctance circuits is greatly improved for given magnet strengths: this enables a very substantial increase in the holding force of the actuator for a given magnet strength and for a given size of actuator. Additionally, the transient power consumed by coils 60,61 to switch the armature from one bistable position to the other is substantially reduced as more efficient flux generation in the yoke takes place. Not
20 only does this result in a substantially reduced current consumption during switching, but it is discovered that substantially shorter current pulse times can be used to effect the switching operation.

25 Improvements in the performance of the device are also found with the use of the "one-piece" outer yoke lamination configuration: that is to say, both the low reluctance path and the high reluctance path of a bistable position are provided in the same structure (ie. in each lamination). This also assists in the transient flux generation by the appropriate coil 60,61.

Traditionally, prior art devices have been constructed around a cylindrical armature with a cylindrical yoke, or separate yokes radially spaced around the outside of the cylindrical armature. A substantial advantage in the particular geometrical configuration of actuator illustrated in the figures is that devices of varying specification can be manufactured using standard parts. By increasing the number of laminations 14,15 used, the number of magnets 30 used, and the length of armature, the device is expandable along the axis perpendicular to the plane of the laminations. This permits any desired size of device to be manufactured, and increasing length provides greater and greater holding force of the finished actuator. Thus, actuators can readily be manufactured to provide just sufficient holding force for any particular application, while avoiding the necessity of using substantially over-specified devices which use more current than strictly necessary for the application. It will be understood that in similar manner to the lamination of the yoke, the armature 40 could also be laminated in similar manner for optimum versatility.

In practice, it is not essential to use an inner yoke 31,32 providing that some means to attach the magnets to the outer yoke is provided.

20

An additional preferred feature is the provision of the armature in two halves 40a, 40b as shown in figure 2. This considerably eases the assembly of the actuator. When constructing an actuator, very considerable forces must be overcome to place magnets and armature in position to complete the magnetic circuits. It is preferable to assemble the actuator with unmagnetised "permanent magnets". The two armature halves have a "slug" of high permeability material introduced between them and are then slid into position between the respective upper and lower pole portions 16,17 of the outer yoke 12. The slug effectively expands the armature sufficiently so that the air gap 62 is eliminated. The

30

remaining parts of the actuator are assembled, with the exception of actuator rod 42. Magnetisation of the magnets 30 then takes place by energising both coils in such a way that the desired polarity of magnets 30 are created.

5

The slug is then removed, and the actuator rod 42 is passed through the upper pole portion 16 of the yoke and into a preformed hole in the upper half of the armature. The lower end of the actuator rod 42 is threaded, as is the corresponding preformed hole in the lower half of the armature. The two halves of the armature may thus be brought together by screw threading the actuator rod into the hole in the lower half of the armature. Thus, the necessary mechanical advantage to overcome the magnetic forces is provided by suitable torque on the actuator rod 42.

10
15

CLAIMS

A bistable permanent magnet actuator comprising:
a magnetic yoke having a laminated structure;
at least one permanent magnet; and
5 an armature axially reciprocable in a first direction within the yoke;
the actuator configured to provide:

a first low reluctance flux path and a first high reluctance flux path
when the armature is in a first position;

a second low reluctance flux path and a second high reluctance flux
10 path when the armature is in a second position;

means to drive the armature between the first and second positions;
characterized in that:

each laminate of the yoke defines a plane in which a portion of the
permanent magnet and armature reside, and wherein the configuration of
15 the actuator thereby enables an increase in the permanent magnet flux
flowing through the actuator by the addition of further yoke laminations
and a corresponding increase in the linear dimension of the magnet and
armature in a second direction perpendicular to the plane of the
laminations.

20

2. A bistable permanent magnet actuator according to claim 1 wherein
each laminate of the yoke provides a part of both said low reluctance path
and said high reluctance path.

25 3. A bistable permanent magnet actuator according to claim 1 wherein
each laminate of the yoke entirely encircles the magnet and armature.

4. A bistable permanent magnet actuator according to claim 1 wherein
the armature comprises a laminate structure in which the laminations of
30 the armature are substantially parallel to the laminations of the yoke.

5. A bistable permanent magnet actuator according to claim 4 further

including a plurality of permanent magnets positioned longitudinally in said second direction.

5 6. A bistable permanent magnet actuator according to claim 4 wherein the first and second directions are mutually orthogonal.

7. A bistable permanent magnet actuator according to any preceding claim wherein the means to drive the armature between the first and second positions comprises:

10 a first and a second electric coil each adapted to generate transient magnetic fields in response to a respective actuation signal

wherein the magnetic field generated by the first coil increases the flux in the first high reluctance path without reducing the flux through the permanent magnet, and at the same time reduces the flux in the first low reluctance path, and

15 wherein the magnetic field generated by the second coil increases the flux in the second high reluctance path without reducing the flux through the permanent magnet, and at the same time reduces the flux in the second low reluctance flux path.

20 8. A bistable permanent magnet actuator according to claim 1 wherein the armature is formed in two halves defined by division of the armature by a plane orthogonal to said first direction.

25 9. A bistable permanent magnet actuator according to claim 8 in which the two halves of the armature are held together by an actuator rod passing through the yoke.

10. A method of manufacturing a bistable permanent magnet actuator comprising the steps of:

30 constructing a magnetic yoke from a plurality of laminations each configured to form a part of a magnetic circuit with at least one permanent

magnet and an armature axially reciprocable in a first direction within the yoke;

5 configuring the actuator to provide a first low reluctance flux path and a first high reluctance flux path when the armature is in a first position and a second low reluctance flux path and a second high reluctance flux path when the armature is in a second position;

providing means to drive the armature between the first and second positions; and

10 using a predetermined number of laminations to expand the device in a linear direction orthogonal to the plane of the yoke laminations, and increasing the corresponding linear dimension of the magnet(s) and armature in order to increase in the permanent magnet flux flowing through the actuator to achieve the desired specification of actuator.

15 11. A method of manufacturing a bistable permanent magnet actuator according to claim 10, further comprising the steps of :

forming the armature in two halves by division of the armature by a plane orthogonal to said first direction;

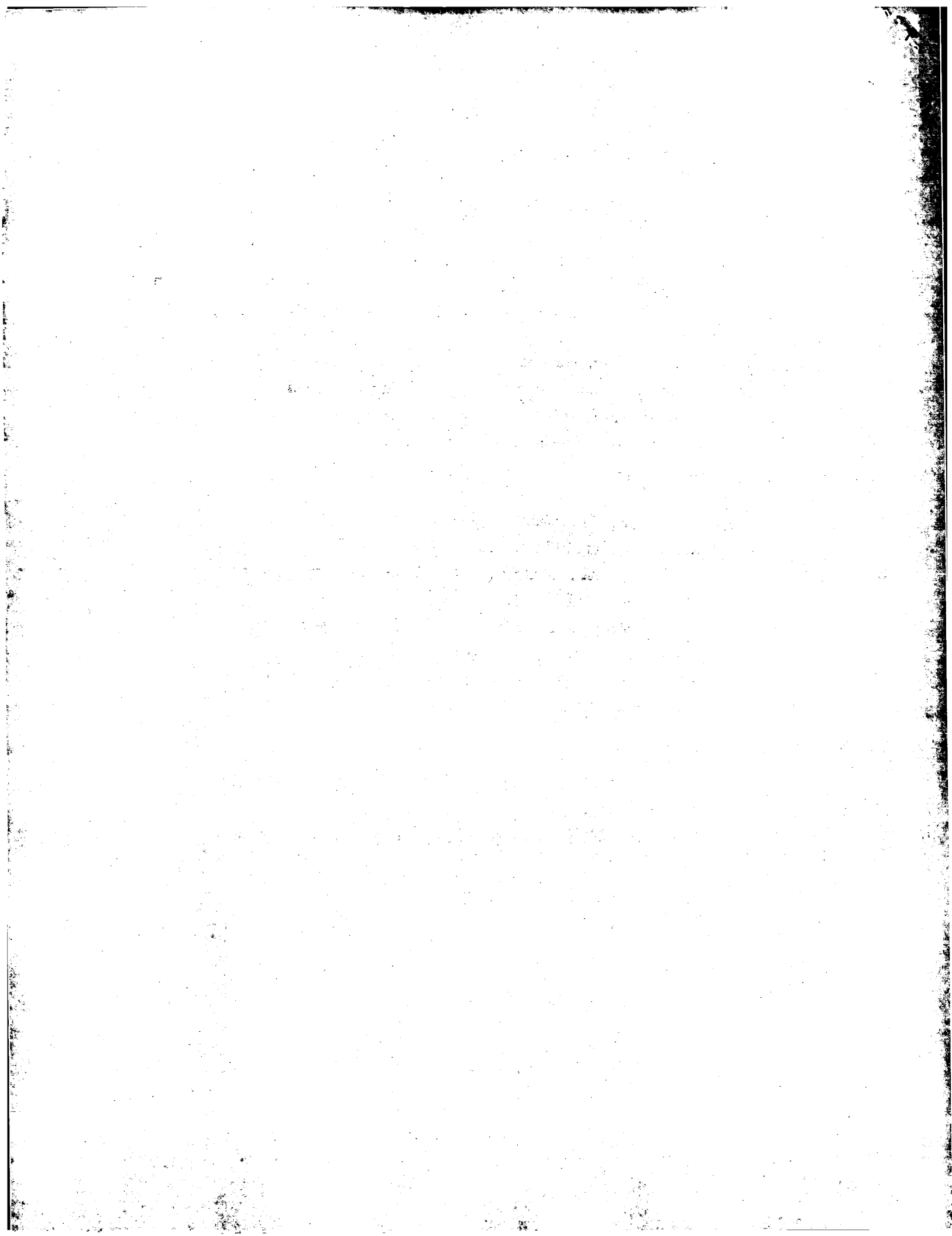
20 introducing a slug of high permeability material between the two halves of the armature and installing the armature and slug into the yoke;

removing the slug and installing an actuator rod adapted to draw together said two armature halves in a direction parallel to said first direction.

25 12. A method of manufacturing a bistable permanent magnet actuator according to claim 11, further comprising the steps of :

installing the at least one permanent magnet in an unmagnetised state;

30 after installation of the armature and slug, and before removal of the slug, magnetising the at least one permanent magnet in situ.



The application was originally made under the Patent Cooperation Treaty with the Japanese Patent Office acting as the receiving office on (86) 30 Apr 1982, being given an application number PCT/JP82/00147. The application was searched by the Japanese Patent Office acting as the International Search Authority (ISA), and published by the International Bureau on (87) 11 Nov 1982 under serial number WO 82/03944 in the Japanese language. The text of the application is contained in the publication made by the International Bureau as above identified, the accompanying text being an English translation thereof.

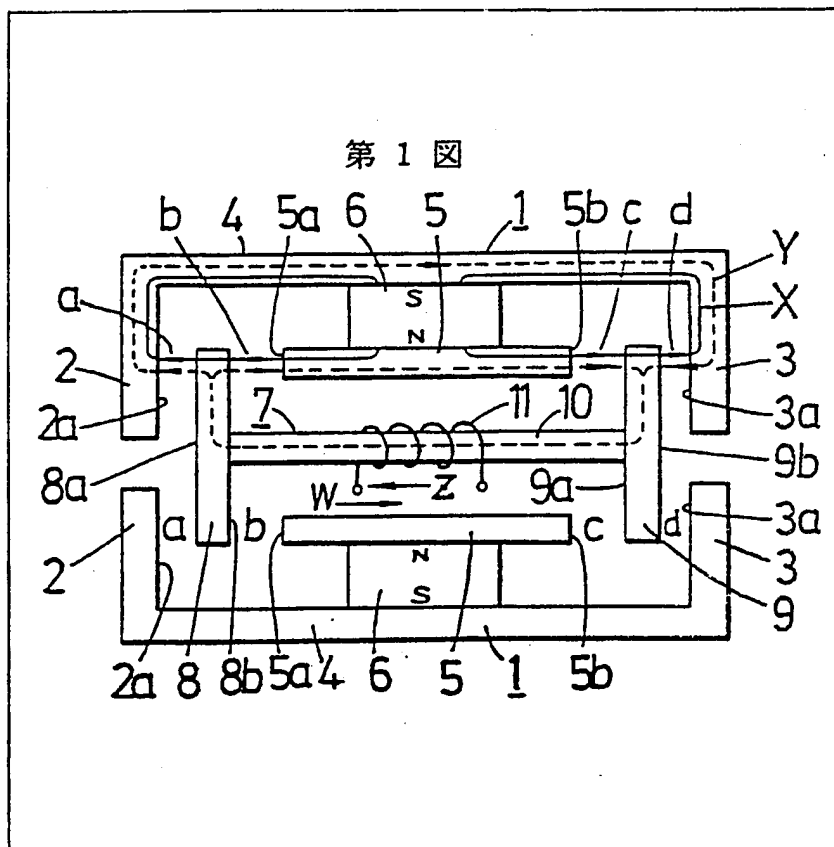
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 JP, A, 56-36109
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 (71) Applicant
 Matsushita Electric Works
 Limited
 (Japan),
 1048 Oaza-Kadoma,
 Kadoma-shi, Osaka 571,
 Japan
 (72) Inventor
 Hidetoshi Matsushita
 (74) Agent and/or Address for
 Service
 D. Young and Co.,
 10 Staple Inn, London
 WC1V 7RD

(54) Polarized electromagnetic relay

(57) A polarized electromagnetic relay is composed of a yoke section having air gaps at four diagonal positions and an H-shaped armature block (7) having four armature portions which are positioned in the air gaps of the yoke section, respectively, and are arranged to enable a parallel movement. The yoke section is composed of two yoke units, each of which is composed of a first pole piece (1) approximately U-shaped, a permanent magnet (6) having the one pole positioned over the center of the lower surface of

the first pole piece, and a second pole piece (5) which contacts the other pole of the permanent magnet (6) and forms air gaps between both ends thereof and both free ends of the first pole piece (1), respectively. In the polarized electromagnetic relay of the invention, the armature block is a lightweight moving element because it contains no permanent magnet and the magnetic flux path in the electromagnetic coil includes no permanent magnet with resultant high magnetic efficiency, so that the operational speed is high, the sensitivity is good and the mechanism operates with less impact.



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